



t lyst. T i es e i t isti s (i ., e esitie i e-  
 st t ), t t i i fl e t fi l i est t  
 (i ., l y t i ss, f ts) of t 3DG. B si s, t  
 t 3DG i i t t e e t i s f e t t l t l t  
 (i ., e esity, e si s, f lity). H e , est of t e es  
 t l t l t s y e t i e l t e s i ffi lty  
 i e sly l t i e esity, f e i st , t e i l Ni f e  
 lly st e esity y e l y e t e l f e i t  
 e t t, t s s tly e t i 3DG s e s e e t e l e f e  
 s e i i e s e i f t s f e s i f i f t i e l s i 17,18].  
 H e , it is e f ssity t e l e t l t l t s, i  
 i s l y i l t f e e t e i e s t s t e i 3DG i t  
 t l st t s s t l f e s 19].

S l t i l s l t i (SLM), s i e t i i t i  
 f t i (AM) t e l e y, i s t i l l y s i f e t f i t i e  
 e f s e l s t i t / e i s t - i s i e l (3D) t l t l t s  
 i t t t s e f e l i t y i s i , f f i i y i e t i e  
 f l i lity of *in-situ* f t i i lity. T e t , e s  
 s s e t SLM e e s s t t s e f T i l l e y s 20],  
 s t i l s l l e y s 21], N i l l e y s 22]. C i s t e s t i l y s f e l /  
 s s t t f e l - s y t s i i s t t - e f t - t -  
 s i s t i l s. C e i t N i e e t s s t t,  
 e i s s e s i l s s t t f e e t  
 i CVD t e t l e e s t t i e l l (< 0.001 t.%)  
 e t e s s s l f - l i t i e f e , i t t e t i -  
 lity s i l l y i t l s 23]. W i l N i s  
 i e s e l i lity (> 0.1 t.%) 17], t i f i l s t  
 t e f e s e f s s i e i t i e 24]. H e , -  
 s i SLM e f e i s s t i l l i t s i f y s e f i s f f i t  
 t i f e e s l t i i f e i t s i t i s i i t l  
 e t i lity f l t i lity t e s e e l s l t  
 (1000–1100 ). F i t i e e f i s e s e s f f e l s  
 i SLM i s s t i l l f i y l l s 25].

T e e e l i t i e s, f e t f i s t t i e e s  
 f s i l e t t e - e t e e 3DG/ e (3DG/C) s t -  
 t s i SLM s i l t e sly i e i t i e i t CVD e t e f  
 . A l l - s i y e i - t y e e s e t l t s  
 i t i l l y i s t i t i SLM f e i e s t t l e l t i e t e -  
 e s e i f e , s i l l y i t s t t e i s e t e y -1.3 45.13, e . l t 20-37 e i lity /T1 (l s441( 250.7( s i t 288.5(t i )-290

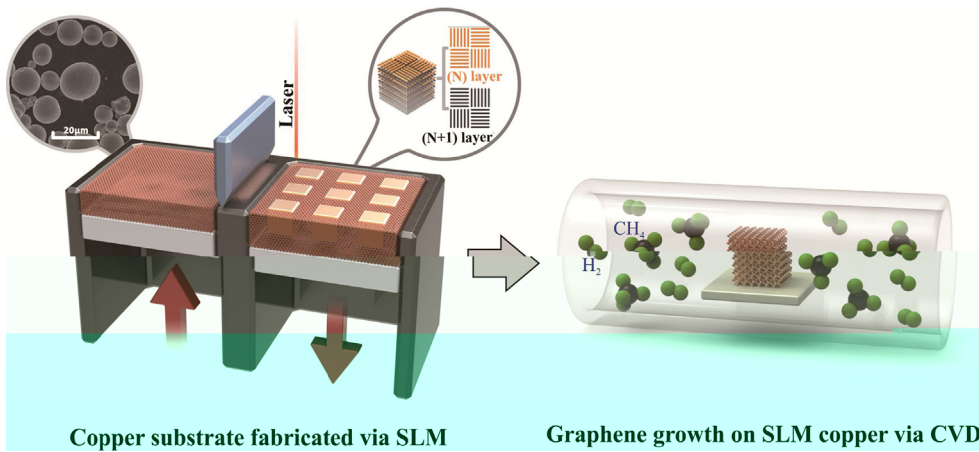


Fig. 1. Illustration of the 3DG/C process: (a) SLM fabrication of copper substrate; (b) in-situ CVD growth of graphene on SLM copper.

ASTM B193-2002 (2002) and ASTM B193-2013 (2013) for tensile strength. The yield strength is 200 MPa (5 × 10<sup>3</sup> psi) for ASTM B193-2013. The tensile strength is 514 MPa (74,000 psi) for ASTM B193-2002. The yield strength is 200 MPa (29,000 psi) for ASTM B193-2013. The tensile strength is 514 MPa (74,000 psi) for ASTM B193-2002. The yield strength is 200 MPa (29,000 psi) for ASTM B193-2013. The tensile strength is 514 MPa (74,000 psi) for ASTM B193-2002. The yield strength is 200 MPa (29,000 psi) for ASTM B193-2013.

### 3. Results and discussion

#### 3.1. Formation of SLM copper

##### 3.1.1. SLM manufacturing of copper under different line energy densities

The test results are shown in Fig. 2. Different scanning speeds and laser powers were used to fabricate copper substrates.

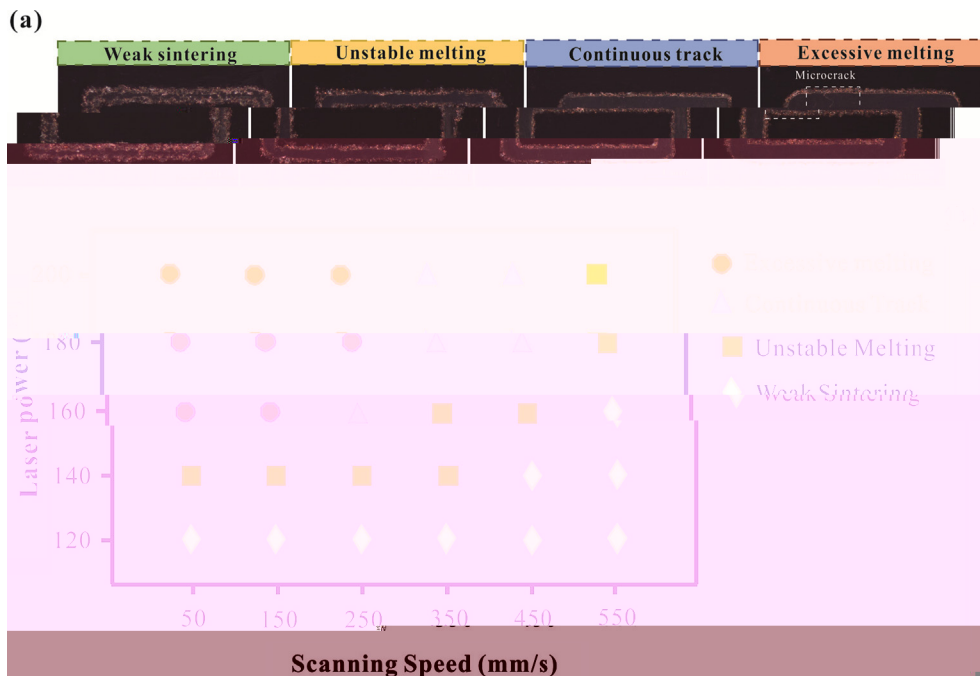


Fig. 2. (a) Typical SEM images of copper substrates fabricated by SLM; (b) Laser power vs. scanning speed for different states of copper substrate.

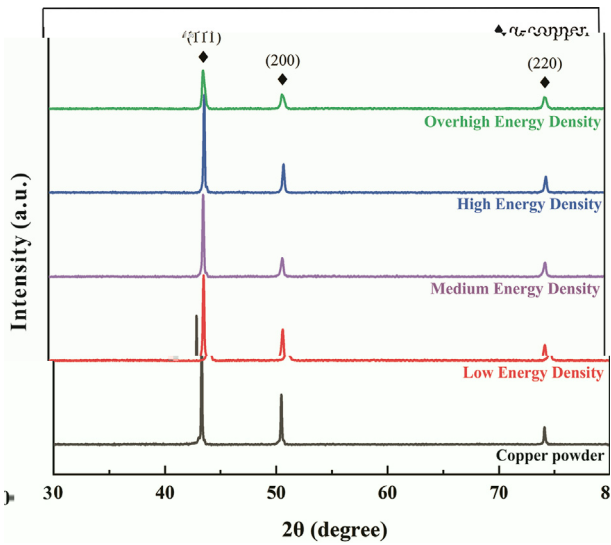


Fig. 3. XRD patterns of copper powder at different energy densities. (a) Overhigh energy density (3000 J/cm<sup>3</sup>), (b) High energy density (857 J/cm<sup>3</sup>), (c) Medium energy density (285 J/cm<sup>3</sup>), (d) Low energy density (128 J/cm<sup>3</sup>), (e) Copper powder.

3.1.2. Formation of anisotropic microstructure under different volumetric energy density

The XRD patterns of copper powder at different energy densities are shown in Fig. 3. The (111) and (200) peaks are observed at 2θ = 43.32° and 50.45°, respectively (Fig. 3). The (111) peak is the most intense peak. The intensity of the (111) peak is significantly higher than that of the (200) and (220) peaks. This indicates that the (111) plane is the preferred orientation of copper powder. The intensity of the (111) peak increases with increasing energy density, indicating that the (111) plane becomes more dominant as the energy density increases.

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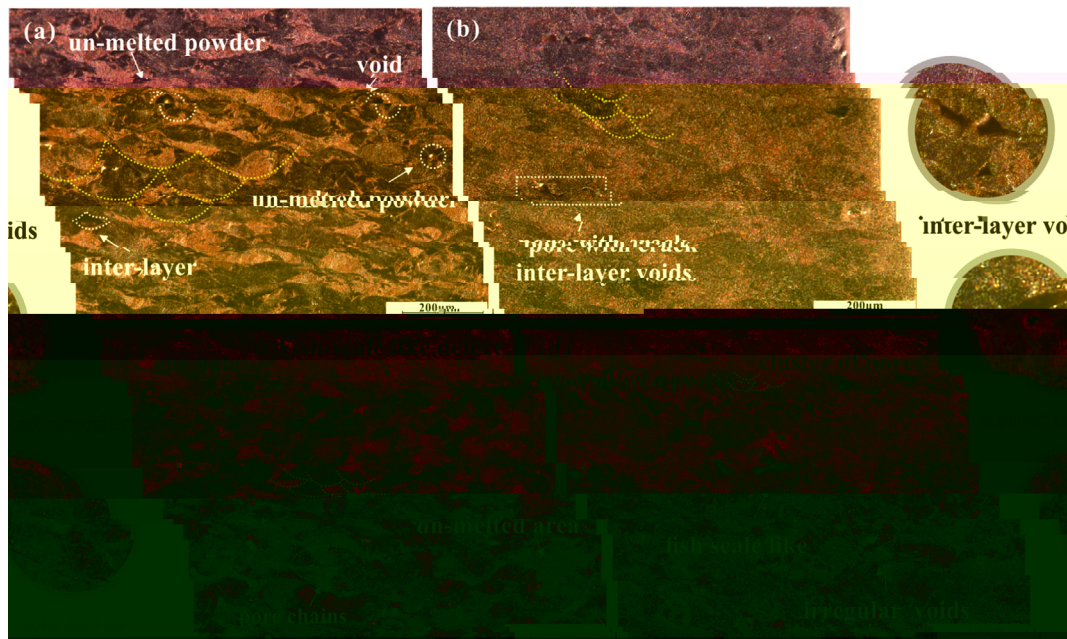


Fig. 4. SEM micrographs of copper powder at different energy densities: (a) 3000 J/cm<sup>3</sup>, (b) 857 J/cm<sup>3</sup>, (c) 285 J/cm<sup>3</sup>, (d) 128 J/cm<sup>3</sup>, (e) Copper powder. (a) un-melted powder, (b) inter-layer voids, (c) pores with cracks, (d) inter-layer voids.

t i t e t e t s e i e i e t.

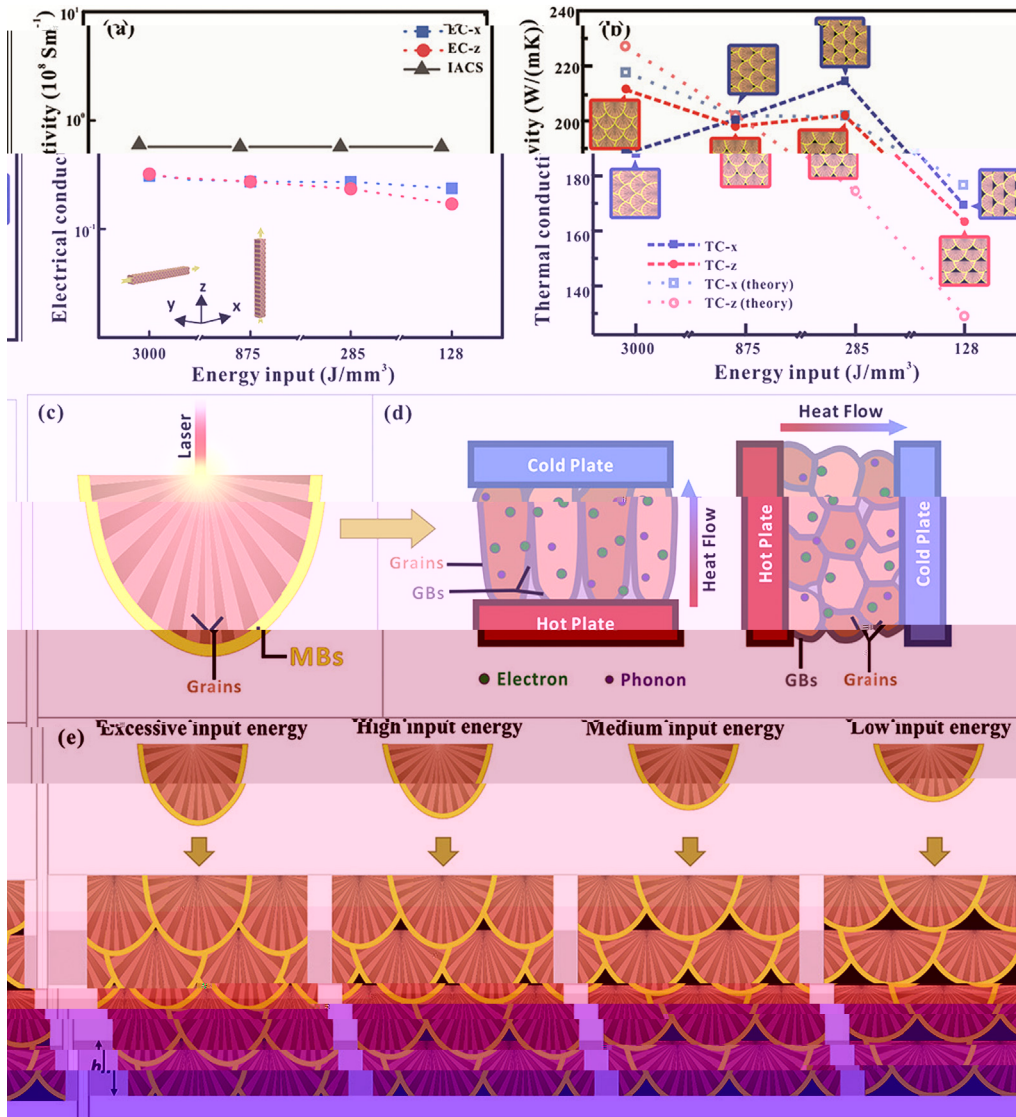


Fig. 7. (a) Electrical conductivity vs energy input; (b) Thermal conductivity vs energy input; (c) Schematic of laser irradiation on the porous scaffold; (d) Schematic of heat conduction through the porous scaffold; (e) Schematic of grain growth at different energy input levels. (Electron and phonon transport are also shown).

The porous scaffold structure is shown in Fig. 7c. The porous scaffold is composed of interconnected porous structure. The porous structure is composed of interconnected porous structure. The porous structure is composed of interconnected porous structure.

3.3. Morphology and structure of CVD 3DG/Cu porous scaffolds

The porous scaffold structure is shown in Fig. 7c. The porous scaffold is composed of interconnected porous structure. The porous structure is composed of interconnected porous structure. The porous structure is composed of interconnected porous structure.

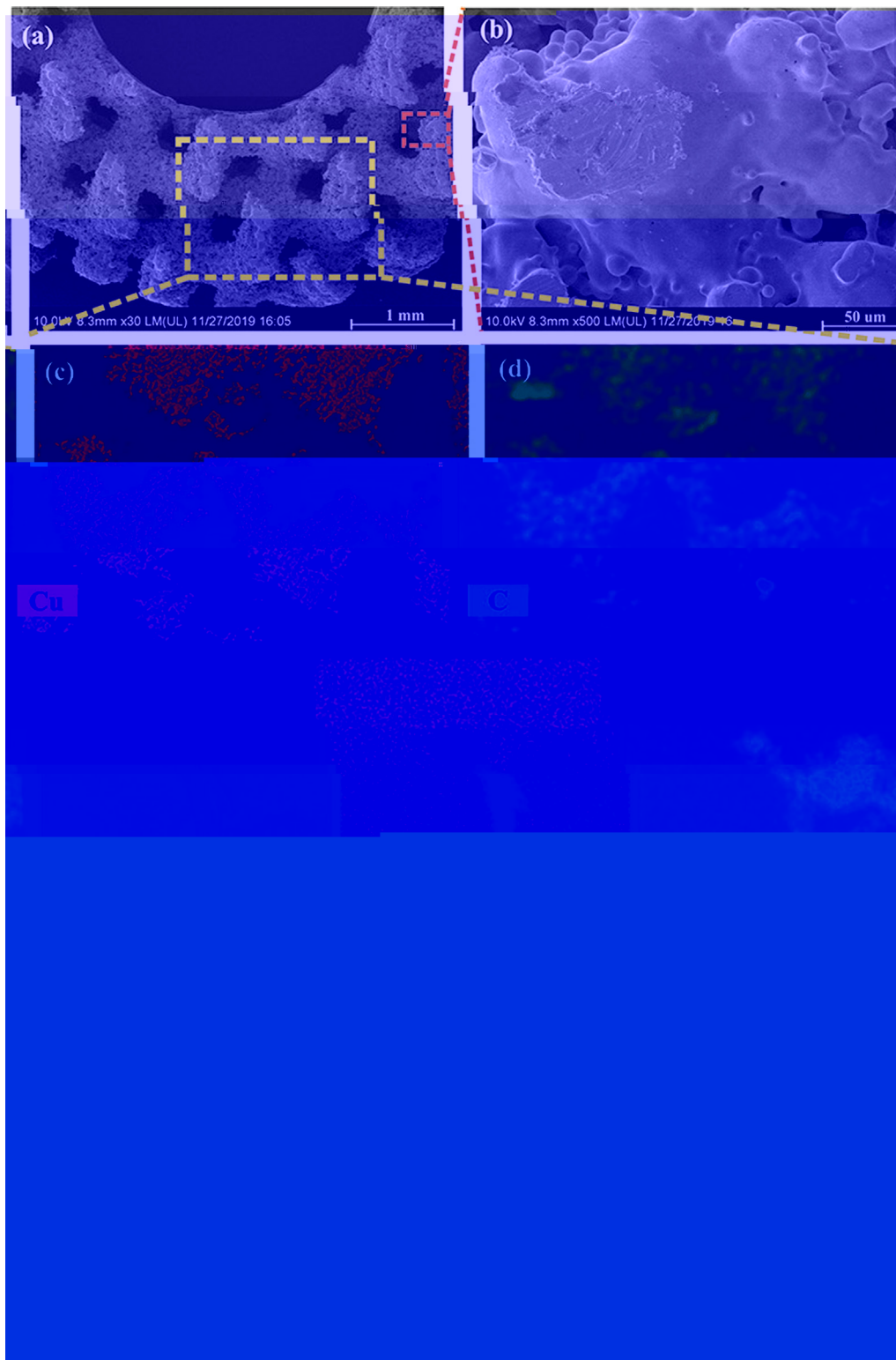


Fig. 8. (a) SEM image of 3DG/C porous scaffold; (b) SEM image of 3DG/C porous scaffold; (c) EDS image of Cu; (d) EDS image of C. (a) SEM image of 3DG/C porous scaffold; (b) SEM image of 3DG/C porous scaffold; (c) EDS image of Cu; (d) EDS image of C.

The density of foams. With respect to the density of foams, the ratio of  $I_D/I_G$  is in the range of 0.71 to 0.93, indicating that the foams are highly porous. The results of the XRD analysis are shown in Fig. 9. As shown in Fig. 9, the diffraction peaks of the foams after 1000 °C, the treatment of  $CH_4$  for 30 s, and the treatment of 20 min of 3DG/C porous scaffold.

### 3.4. Thermal property and EMI shielding effectiveness of 3DG/Cu porous scaffolds

The thermal stability of the porous scaffolds was evaluated by TGA. The results of the TGA analysis are shown in Fig. 10. The weight loss of the porous scaffold after 26.8% is due to the treatment of the porous scaffold.

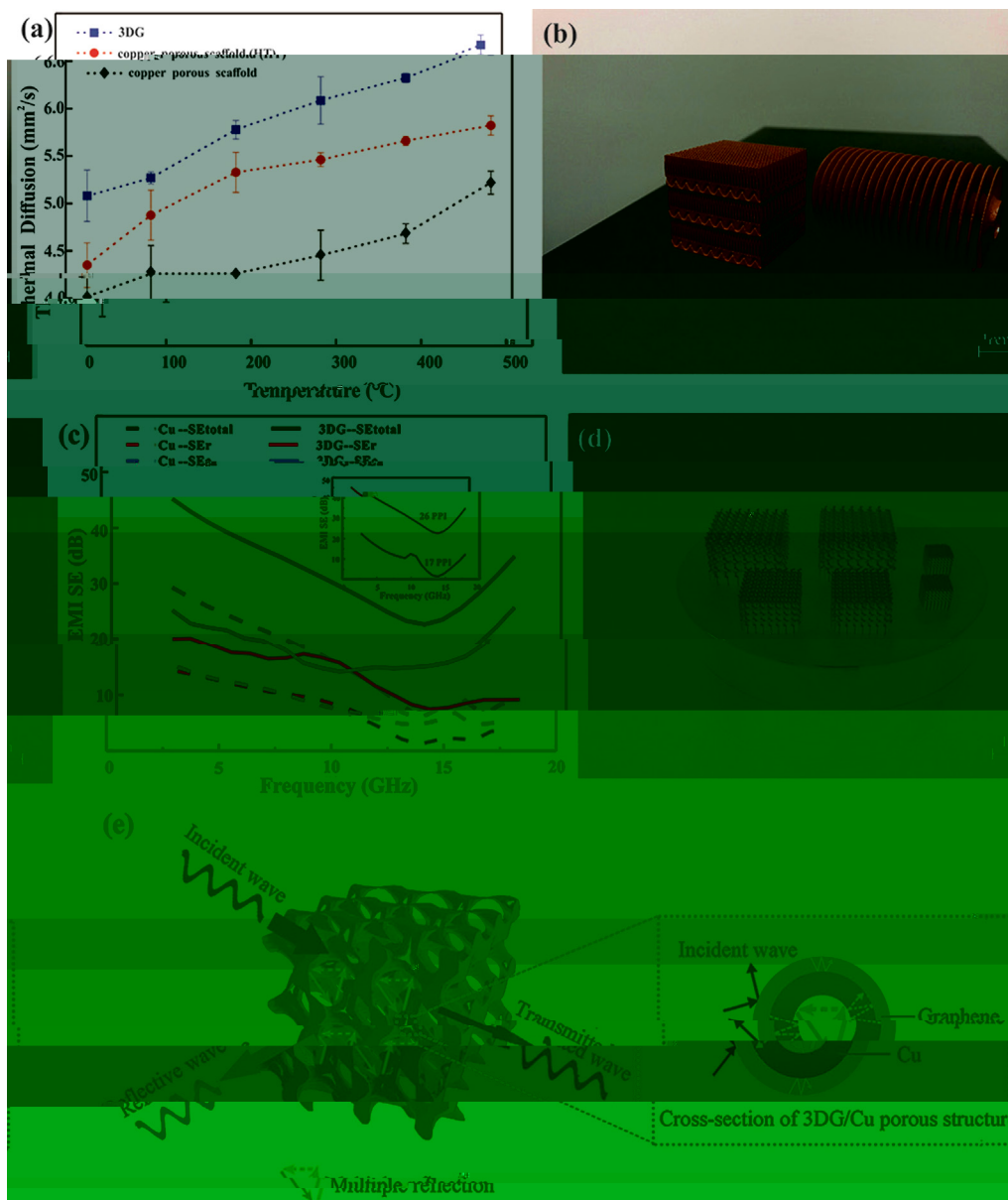


Fig. 9. Performance of 3DG/C porous scaffold: (a) thermal diffusion; (b) SLM prepared porous scaffold; (c) EMI SE; (d) Cross-section of porous structure; (e) Schematic of 3DG/C porous EMI. (For interpretation of the references to this figure legend, the reader is referred to the web version of this article.)

Table 1

Comparison of the performance of porous structures with different porous materials for EMI shielding. The data are taken from the literature.

Coating materials	Substrate	Method	Maximum shielding efficiency (dB)	Improvement of thermal property (%)	Ref
G	PPS	Infiltration + freeze-drying + sintering	37	-	50]
G	PS	Hydrothermal synthesis + sintering	29.3	-	56]
G	PMMA	Sol-gel + freeze-drying + sintering	19	-	57]
C /G	/C	Sf + infiltration + freeze-drying	-	8.5	58]
G	Ni	Freeze + CVD	-	554	59]
G	C-Ni	Electroless plating + freeze-drying	20	-	60]
G	C	Precipitation + CVD	-	2.4	61]
G	PPS	Freeze-drying + freeze-drying	47	6.3	62]
G	C	CVD + SLM	47.8	27	This work

Note: PPS (poly (styrene)-PPMA, polystyrene-PS.





Declaration of Competing Interest

The authors declare that they have no competing interests.

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Appendix A. Supplementary data

Supplementary data for this article is available at <https://doi.org/10.1016/j.jheale.2020.105904>.

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